EVE 402/502 Air Pollution Generation and Control

Chapter #4
Dispersion of Pollutants
In the Atmosphere

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"Transport and dilution of pollutants by air motions goes on constantly; and all of humanity, particularly that large segment inhabiting cities and industrial areas, depends strongly on this capability of the air to carry away and dilute the pollutants it receives. What we call "air pollution" occurs when too much waste material is emitted into an air volume for the air's capacity to carry it away and dilute it. Thus we must...understand the atmospheric mechanisms that result in transport and dilution..."

F. A. Gifford, 1975

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Introduction

- Atmospheric dispersion depends on
 - Physical/chemical nature of emissions
 - Meteorological characteristics
 - Stack location
 - Terrain downwind from stack
- No analytical method for estimating dispersion accounts for all of the above

Classifications of AQ Models

- Developed for a number of pollutant types and time periods
 - Short-term models for a few hours to a few days; worst case episode conditions
 - Long-term models to predict seasonal or annual average concentrations; health effects due to exposure
- Classified by
 - Non-reactive models pollutants such as SO₂ and CO
 - Reactive models pollutants such as O₃, NO₂, etc.

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Regulatory Application of Models

- PSD: Prevention of Significant Deterioration of Air Quality in relatively clean areas (e.g. National Parks)
- SIP: State Implementation Plan revisions for existing sources and to New Source Reviews (NSR)





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Characteristics of Dispersion Models

- The accuracy of dispersion models varies according to the complexity of the terrain and the sufficiency of historic meteorological data.
- The acceptability of the results of dispersion models varies with the experience and viewpoint of the modeler, the regulator and the intervener.

Gaussian Dispersion Models

- · Most widely used
- · Based on the assumption
 - plume spread results primarily by molecular diffusion
 - horizontal and vertical pollutant concentrations in the plume are normally distributed (double Gaussian distribution)

Plume spread and shape vary in response to meteorological conditions

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Characteristics of Pollutant Plume

- Horizontal (y) and vertical (z) dispersion, is caused by eddies and random shifts of wind direction.
- · Key parameters are:
 - Physical stack height (h)
 Plume rise (Δh)
 - Effective stack height (H) Wind speed (u_x)

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Model Assumptions

- Gaussian dispersion modeling based on a number of assumptions including
 - Steady-state conditions (constant source emission strength)
 - Wind speed, direction and diffusion characteristics of the plume are constant
 - Mass transfer due to bulk motion in the x-direction far exceeds the contribution due to mass diffusion
 - Conservation of mass, i.e. no chemical transformations take place
 - Wind speeds are ≥1 m/sec.
 - Limited to predicting concentrations > 50 m downwind

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Gaussian Dispersion Equation – elevated source

$$C(x, y, z) = \frac{Q}{2\pi\sigma_y\sigma_z\overline{u}} \exp\left[-\frac{1}{2}\left(\frac{y^2}{\sigma_y^2} + \frac{(-H)^2}{\sigma_z^2}\right)\right]$$

Why isn't x in the equation?

 $\sigma_{_{\! V}}$ and $\sigma_{_{\! Z}}$ depend on the atmospheric conditions

Atmospheric stability classifications are defined in terms of surface wind speed, incoming solar radiation and cloud cover

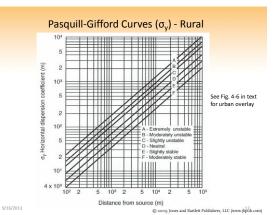
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Key to Stability Categories

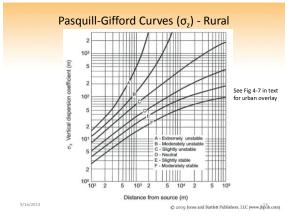
Figure 3-1

Surface	Day Incoming Solar Radiation			Night ation Cloudiness ^e	
Wind Speed ^a m/s	Strongb	Moderate ^c	Slight ^d	Cloudy (≥4/8)	Clear (≤3/8)
<2	A	A-B ^f	В	E	F
2-3	A-B	В	C	E	F
3-5	В	B-C	C	D	E
5-6	С	C-D	D	D	D
>6	С	D	D	D	D

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To determine σ_y and σ_z

- Pasquill-Gifford Curves
 - Figure 4-6 (σ_{v} , urban and rural)
 - Figure 4-7 (σ_z , urban and rural)
- The curves aren't necessarily easy to read, though
 - Equations 4-12 through 4-14
 - Table 4-1 and 4-2
- McElroy-Pooler (Urban)
 - Table 4-3 and Table 4-4

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The figures and correlations for estimating the dispersion coefficients correspond to sampling times of approximately 10 min. Regulatory models now assume 1 or 8 hour averages

• Variation of concentration with averaging time: $C_t = C_{10}(10/t)^q \ , \ \text{where} \ q = 0.17 - 0.20$

So, determine downwind concentration using model (C_{10}), then use equation above to determine concentration (C_{t}) for appropriate averaging time (t)

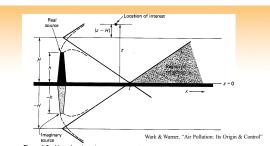


Figure 4-3 Use of an imaginary source to describe mathematically gaseous reflection at surface of the earth.

reflection at surface of the earth.
$$C (y,z) = \frac{Q}{2\pi\sigma_{y}\sigma_{z}\overline{u}} \exp\left[-\frac{y^{2}}{2\sigma_{y}^{2}}\right] \exp\left[-\frac{(-H)^{2}}{2\sigma_{z}^{2}}\right] + \exp\left[-\frac{(+H)^{2}}{2\sigma_{z}^{2}}\right]$$

What if the surface is absorbing?

How should the concentration profile look w/ reflection?

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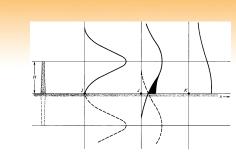


Figure 4-4 Effect of ground reflection on pollutant concentration downwind

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Elevated source with reflection (Eqn 4-8)

$$C(x, y, z) = \frac{Q}{2\pi u \sigma_y \sigma_z} \left[\exp\left(-\frac{y^2}{2\sigma_y^2}\right) \right] \left\{ \exp\left[-\frac{z - H^2}{2\sigma_z^2}\right] + \exp\left[-\frac{z + H^2}{2\sigma_z^2}\right] \right\}$$

where C(x,y,z) = time averaged contaminant concentration,

Q = source emissions strength, g/s

u = mean wind speed at the effective stack height, m/s

 $\sigma_{\!\scriptscriptstyle y}$ = dispersion coefficient in the crosswind direction, m

 σ_z = dispersion coefficient in the vertical direction, m

y = horizontal distance from centerline, m

z = vertical distance from centerline, m

H = effective stack height = $h + \Delta h$

h = stack height, m

 $\Delta h = plume rise, m$

The model assumes that there is a continuous point source emission, crosswind and vertical dispersion are Gaussian in nature, plume moves downwind at a rate equal to u, no particles settle out, downwind dispersion is negligible compared to the bulk wind motion, and that the pollutants are inert_{© 2009 Joses} and Bardles Publishers, LLC (www.lprub.com)

$$C(x, y, z) = \frac{Q}{2\pi u \sigma_y \sigma_z} \left[\exp\left(\frac{y^2}{2\sigma_y^2}\right) \right] \left\{ \exp\left[\frac{-z - H^2}{2\sigma_z^2}\right] + \exp\left[\frac{-z + H^2}{2\sigma_z^2}\right] \right\}$$

The maximum downwind concentration will occur on the plume centerline where y = 0 Assuming an elevated source, Equation 4-8 simplifies to:

$$C(x,0,z) = \frac{Q}{2\pi u \sigma_y \sigma_z} \left\{ \exp \left[\frac{-z - H^2}{2\sigma_z^2} \right] + \exp \left[\frac{-z + H^2}{2\sigma_z^2} \right] \right\}$$

Many receptors of concern will be located at ground level such that z=0. With an elevated source, the downwind, ground level concentration can be estimated as follows:

$$C(x, y, 0) = \frac{Q}{\pi u \sigma_y \sigma_z} \exp\left(\frac{-y^2}{2\sigma_y^2}\right) \exp\left(\frac{-H^2}{2\sigma_z^2}\right)$$

The ground level concentration, occurring on the center line is easily determined by substituting y = 0 the above equation

$$C(x,0,0) = \frac{Q}{\pi u \sigma_y \sigma_z} \exp \left(\frac{-H^2}{2\sigma_z^2} \right)_{\text{0 20 by Jones and Bartlett Publishers, LLC (www.jbpub.com}}$$

Finally, if a ground level source such as a landfill is assumed, the effective stack height can be modeled as H = 0. If the center line, ground level concentration is desired, the previous equation is simplified as follows:

$$C(x,0,0) = \frac{Q}{\pi u \sigma_{v} \sigma_{z}}$$

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Maximum Ground Level Concentration

Under moderately stable to near neutral conditions, $\sigma_y = k_1 \sigma_z$

The ground level concentration at the center line is

$$C(4,0,0) = \frac{Q}{\pi k_1 \sigma_z^2 u} \exp \left[-\frac{H^2}{2\sigma_z^2} \right]$$

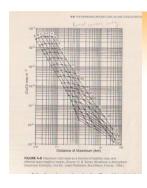
The maximum occurs at

$$dC/d\sigma_z = 0 \quad \Rightarrow \sigma_z = \frac{H}{\sqrt{2}}$$

Once $\boldsymbol{\sigma}_{\!z}$ is determined, x can be known and subsequently C.

$$C (0,0,0) = \frac{Q}{\pi \sigma_y \sigma_z u} \exp \left[1 \right] = 0.1171 \frac{Q}{\sigma_y \sigma_z u}$$

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Alternate Method to Find Max GL Conc Figure 4-8 (Rural only)

A general equation was fit to the data so the solution can be found algebraically.

Equation 4-15

Table 4-5

$$\left(\frac{Cu}{Q}\right)_{\max} = \exp\left[a+b \ln H + c \ln H^2 + d \ln H^3\right]_{\text{@ 2009 Jones and Bartlett Publishers, ILC (www.jbpub.com)}}$$

Plume Rise (Δh) equations are usually expressed as a function of:

- Momentum term accounts for vertical momentum of stack gas due to its own velocity
- Buoyancy term accounts for the difference in stack gas and environmental temperatures

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Commonly used empirical equations for plum rise include:

- Carson and Moses (Eqn 4-18)
- Holland Equation (4-19) good for tall stacks
- Thomas Equation (4-21)

Correct Units are Important!!

Briggs Equations Most Commonly Used Table 4-6 provides a flow diagram

Example
LXample
For an overcast winter night, (a) estimate the maximum ground-level SO_2 concentration 10km downwind from a copper smelter if the wind speed is 3 m/s at 10 m. Assume h = 100m, Δh = 150 m, and an urban environment. (b) Estimate the maximum ground-level concentration along the center line. Assume a source strength of 5027 g/s of SO_2 .
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Example
Calculate H using plume rise equations for an 80 m high source (h) with a stack diameter = 4 m, stack velocity = 14 m/s, stack gas temperature = 90°C (363 K), ambient temperature = 25°C (298 K), u at 10 m = 4m/s, and stability class = B. Then
determine MGLC at its location.
:= \h
$\Delta h_{plume\ rise} = H = \sigma_{y} = \sigma_{y} = \sigma_{y}$